## ISOTHERMAL VAPOR-LIQUID EQUILIBRIA FOR BINARY AND TERNARY MIXTURES FORMED BY 1-BUTANOL, ACETONITRILE AND BENZENE

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#### ABSTRACT

Isothermal vapor-liquid equilibrium data are presented for the binary acetonitrile-1-butanol and ternary 1-butanol-acetonitrile-benzene systems at 60°C. The experimental results are well correlated with the UNIQUAC associated-solution model.

#### INTRODUCTION

Studies on the thermodynamic properties of 1-butanol solutions are currently under way in this laboratory. A literature survey [1-5] showed that isothermal vapor-liquid equilibrium (VLE) data for ternary systems containing 1-butanol are a very few. This work presents isothermal VLE data for the systems acetonitrile-1-butanol and 1-butanol-acetonitrile-benzene at 60°C. The VLE data for the two binary systems constituting the ternary system had been measured: acetonitrile-benzene at 45°C [6] and 1-butanol-benzene at 45°C [7]. The measured results are well correlated with the UNIQUAC associated-solution model [8].

### **EXPERIMENTAL**

Acetonitrile and 1-butanol (Nakarai Pure Chemical Industries Ltd., Analytical reagent grade) were used without further purification. C.P. benzene was subjected to repeated recrystallization. An Anton Paar densimeter (DMA40) was used to measure densities of the compounds. Gas chromatographic analysis did not detect any appreciable impurities in the chemicals. Table 1 shows values of densities and vapor pressures of the compounds, together with literature values [6,9].

An all-glass Boublik vapor-recirculation still [10] was used to obtain the VLE data. Refractive index measurements were carried out for composition

Compound	Density at 2	$25^{\circ}C (g \text{ cm}^{-3})$	Vapor pres	ssure at 60°C (Torr)
	Obs.	Lit. [9]	Obs.	Lit. [9]
1-Butanol	0.8059	0.8060	59.1	59.01
Acetonitrile	0.7766	0.7766	368.1	368.00(6)
Benzene	0.8736	0.8737	391.5	391.47

TABLE 1

Densities an	d vapor	pressures	of	compounds
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determination of binary vapor and liquid-phase sample solutions by using a Shimadzu refractometer at 25°C. Ternary sample solutions were analyzed by combining use of a gas chromatograph (Shimadzu GC-8A) and an electronic integrator (Shimadzu Chromatopac E-1A). The experimental errors involved in the measured variables were as follows: 0.16 Torr for pressure; 0.05 K for temperature; 0.002 mole fraction for liquid and vapor-phase compositions.

### **RESULTS AND DISCUSSION**

The measured VLE results at  $60^{\circ}$ C are presented for the binary system acetonitrile-1-butanol in Table 2 and for the ternary system 1-butanol-acetonitrile-benzene in Table 3.

The experimental data were reduced by use of the relation

$$P\phi_I y_I = \gamma_I x_I P_I^s \phi_I^s \exp\left[v_I^{\rm L} (P - P_I^s) / RT\right]$$
(1)

where P is the total pressure,  $\gamma$  is the activity coefficient, x and y are the liquid- and vapor-phase mole fractions,  $P^s$  is the pure-component vapor pressure at equilibrium absolute temperature T and  $v^L$  is the pure-liquid molar volume and was calculated from the modified Rackett equation [11].

$x_1$	$y_1$	P (Torr)	$\gamma_1$	γ <sub>2</sub>	$oldsymbol{\phi}_1$	$\boldsymbol{\phi}_2$
0.101	0.690	174.1	3.346	1.008	0.973	0.985
0.237	0.776	231.4	2.110	1.139	0.963	0.983
0.340	0.815	254.3	1.690	1.195	0.959	0.983
0.401	0.819	264.5	1.495	1.339	0.958	0.983
0.551	0.847	292.0	1.236	1.667	0.953	0.983
0.676	0.878	311.1	1.109	1.964	0.950	0.984
0.807	0.916	332.5	1.032	2.436	0.946	0.985
0.968	0.984	362.8	1.003	3.059	0.941	0.989

TABLE 2

Vapor-liquid equilibrium data for the system acetonitrile (1)-1-butanol (2) at 60°C

**TABLE 3** 

Vapor-liquid equilibrium data for the system 1-butanol (1)-acetonitrile (2)-benzene (3) at 60°C

Point	x,	x,	X1	Y,	<i>γ</i> ,	۲, ۲	Р	۲,	۶.	۲.	φ.	¢	φ,
		ı	) 	•	1	5	(Torr)	:	1	ì	-	4	- -
1	0.065	0.647	0.288	0.025	0.587	0.388	461.2	2.937	1.129	1.612	0.972	0.934	0.995
7	0.083	0.843	0.074	0.038	0.804	0.158	388.4	2.971	1.004	2.186	0.980	0.939	1.011
ę	0.189	0.328	0.483	0.054	0.389	0.557	426.9	2.018	1.386	1.266	0.971	0.948	0.986
4	0.548	0.189	0.263	0.124	0.366	0.510	346.3	1.299	1.855	1.733	0.973	0.957	066.0
S.	0.689	0.244	0.067	0.174	0.633	0.193	267.4	1.127	1.924	2.015	0.979	0.960	1.003
9	0.176	0.066	0.758	0.066	0.117	0.817	393.2	2.455	1.951	1.084	0.977	0.969	0.980
7	0.243	0.378	0.379	0.066	0.444	0.490	414.0	1.860	1.329	1.381	0.971	0.946	0.989
×	0.229	0.331	0.440	0.059	0.400	0.541	421.6	1.797	1.395	1.334	0.971	0.948	0.987
6	0.247	0.154	0.599	0.072	0.235	0.693	402.5	1.946	1.702	1.193	0.973	0.959	0.982
10	0.154	0.254	0.592	0.050	0.321	0.629	433.8	2.331	1.506	1.182	0.971	0.951	0.983
11	0.302	0.407	0.291	0.076	0.493	0.431	398.6	1.661	1.319	1.528	0.972	0.946	0.992
12	0.450	0.168	0.382	0.098	0.306	0.596	368.5	1.331	1.858	1.479	0.973	0.958	0.986
13	0.460	0.354	0.186	0.106	0.541	0.353	350.2	1.340	1.469	1.727	0.974	0.950	0.996
14	0.457	0.455	0.088	0.121	0.687	0.192	326.8	1.441	1.354	1.869	0.977	0.950	1.004
15	0.391	0.134	0.475	0.091	0.231	0.678	377.5	1.458	1.808	1.382	0.973	0.962	0.984
$B_{11} = -$	3077 cm <sup>3</sup> n	nol <sup>-1</sup> , $B_{22}$	= - 3475	cm <sup>3</sup> mol <sup>-1</sup>	$B_{11} = -$	1111 cm <sup>3</sup> n	nol <sup>-1</sup> , $B_{12}$	= - 2002 c	m <sup>3</sup> mol <sup>1</sup>	$B_{13} = -9$	019 cm <sup>3</sup> mc	ы '. К	
$B_{23} =$	– 1057 cm <sup>3</sup>	$mol^{-1}, v$	$\frac{1}{3} = 96.53$	cm <sup>3</sup> mol <sup>1</sup>	$v_{2}^{\rm L} = 55.0$	)6 cm <sup>3</sup> mol	$v_3^{\rm L} = \frac{1}{93}$		ol - <sup>1</sup>	-			

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The fugacity coefficients,  $\phi_I$  at P and  $\phi_I^s$  at  $P_I^s$ , were calculated from the relation

$$\ln \phi_I = \left(2\sum_J y_J B_{IJ} - \sum_I \sum_J y_I y_J B_{IJ}\right) \frac{P}{RT}$$
(2)

where the second virial coefficient  $B_{IJ}$  were estimated from the correlation of Hayden and O'Connell [12].

The UNIQUAC associated-solution model [8] gives the activity coefficients of 1-butanol (A), acetonitrile (B) and benzene (C) as follows:

$$\ln \gamma_{A} = \ln\left(\frac{\Phi_{A_{1}}}{\Phi_{A_{1}}^{0}x_{A}}\right) + r_{A}\left(\frac{1}{V_{A}^{0}} - \frac{1}{V}\right) - \left(\frac{Z}{2}\right)q_{A}\left[\ln\left(\frac{\Phi_{A}}{\theta_{A}}\right) + 1 - \frac{\Phi_{A}}{\theta_{A}}\right] + q_{A}\left[1 - \ln\left(\sum_{J}\theta_{J}\tau_{JA}\right) - \sum_{J}\frac{\theta_{J}\tau_{AJ}}{\sum_{K}\theta_{K}\tau_{KJ}}\right]$$
(3)  
$$\ln \gamma_{B} = \ln\left(\frac{\Phi_{B_{1}}}{x_{B}}\right) + 1 - \frac{r_{B}}{V} - \left(\frac{Z}{2}\right)q_{B}\left[\ln\left(\frac{\Phi_{B}}{\theta_{B}}\right) + 1 - \frac{\Phi_{B}}{\theta_{B}}\right] + q_{B}\left[1 - \ln\left(\sum_{J}\theta_{J}\tau_{JB}\right) - \sum_{J}\frac{\theta_{J}\tau_{BJ}}{\sum_{K}\theta_{K}\tau_{KJ}}\right]$$
(4)

and  $\ln \gamma_{\rm C}$  is expressed by changing the suffix B to C in eqn. (4). Z is the coordination number equal to 10. The nominal segment fraction  $\Phi_I$ , the overall surface fraction  $\theta_I$  and the adjustable parameter  $\tau_{JI}$  are indicated by

$$\Phi_{I} = r_{I} x_{I} / \sum_{r} r_{J} x_{J}$$
<sup>(5)</sup>

$$\theta_I = q_I x_I / \sum_J q_J x_J \tag{6}$$

$$\tau_{JI} = \exp(-a_{JI}/T) \tag{7}$$

The true molar volume of the ternary mixture is expressed as

$$\frac{1}{V} = \frac{\Phi_{A_1}}{r_A (1 - K_A \Phi_{A_1})} + \frac{\Phi_{B_1}}{r_B} \left[ 1 + \frac{K_{AB} r_B \Phi_{A_1}}{(1 - K_A \Phi_{A_1})} \right] + \frac{\Phi_{C_1}}{r_C} \left[ 1 + \frac{K_{AC} r_C \Phi_{A_1}}{(1 - K_A \Phi_{A_1})} \right]$$
(8)

The monomeric segment fractions of all the components,  $\Phi_{A_1}$ ,  $\Phi_{B_1}$  and  $\Phi_{C_1}$ , are numerically solved from eqns. (9–11).

$$\Phi_{A} = \frac{\Phi_{A_{1}}}{\left(1 - K_{A}\Phi_{A_{1}}\right)^{2}} \left[1 + r_{A}\left(K_{AB}\Phi_{B_{1}} + K_{AC}\Phi_{C_{1}}\right)\right]$$
(9)

$$\Phi_{\rm B} = \Phi_{\rm B_1} \left[ 1 + \frac{r_{\rm B} K_{\rm AB} \Phi_{\rm A_1}}{\left(1 - K_{\rm A} \Phi_{\rm A_1}\right)} \right]$$
(10)

$$\Phi_{\rm C} = \Phi_{\rm C_1} \left[ 1 + \frac{r_{\rm C} K_{\rm AC} \Phi_{\rm A_1}}{\left(1 - K_{\rm A} \Phi_{\rm A_1}\right)} \right] \tag{11}$$

At pure alcohol state  $\Phi_{A_1}^0$  and  $V_A^0$  are derived from eqns. (12) and (13), respectively.

$$\Phi_{A_1}^0 = \left[ 2K_A + 1 - (1 + 4K_A)^{1/2} \right] / 2K_A^2$$
(12)
$$\frac{1}{K_A} = \left( 1 - K_A \Phi^0 \right) / r$$
(13)

$$\frac{1}{V_{\rm A}^{0}} = (1 - K_{\rm A} \Phi_{\rm A_1}^{0}) / r_{\rm A}$$
(13)

The pure-component structural parameters were calculated according to the method of Vera et al. [13]: for 1-butanol, r = 2.77 and q = 2.42; for acetonitrile, r = 1.50 and q = 1.40; for benzene, r = 2.56 and q = 2.05. The association constant for 1-butanol  $K_A$  is 69.5 at 50°C [14]. The enthalpy of hydrogen-bond formation for the alcohol  $h_A$  is -23.2 kJ mol<sup>-1</sup> [15]. The values of the solvation constant and the enthalpy of complex formation are  $K_{AB} = 40$  at 50°C and  $h_{AB} = -17$  kJ mol<sup>-1</sup> for 1-butanol-acetonitrile and  $K_{AC} = 2.5$  at 50°C and  $h_{AC} = -8.3$  kJ mol<sup>-1</sup> [8].  $h_A$ ,  $h_{AB}$  and  $h_{AC}$  were assumed to be independent of temperature. The temperature dependence of the equilibrium constants were described by the van't Hoff relation.

An optimum set of the parameters for the binary VLE results were obtained by use of a computer program similar to that described by Prausnitz et al. [16]. Standard deviations for the measured variables used in data reduction were  $\sigma_P = 1$  Torr for pressure,  $\sigma_T = 0.05$  K for temperature,  $\sigma_x = 0.001$  for liquid-phase mole fraction and  $\sigma_y = 0.003$  for vapor-phase mole fraction. Table 4 shows the results obtained in fitting the UNIQUAC associated-solution model to the binary VLE results and the root-mean-

System	Tempera-	Number	Root-mean-square deviations Pa				Paramet	Parameters	
	ture (°C)	of data points	δP (Torr)	δ <i>T</i> (K)	$\frac{\delta x}{(\times 10^3)}$	$\frac{\delta y}{(\times 10^3)}$	$\overline{\begin{array}{c}a_{AB}\ (K)\end{array}}$	а <sub>ва</sub> (К)	
Acetonitrile (A)- benzene (B)	45	12	0.78	0.02	0.5	3.6	- 10.54	258.38	
1-Butanol (A)– acetonitrile (B)	60	8	3.71	0.00	1.1	8.1	848.22	82.28	
1-Butanol (A)- benzene (B)	45	9	0.41	0.01	0.2	4.2	129.95	-11.32	

Binary calculated	results of v	vapor-liquid	equilibrium	data	reduction

TABLE 4



Fig. 1. Vapor-liquid equilibria for: (a) acetonitrile (1)-benzene (2) at  $45^{\circ}$ C; (b) 1-butanol (1)-benzene (2) at  $45^{\circ}$ C; (c) acetonitrile (1)-benzene (2) at  $60^{\circ}$ C. (----) Calculated. (•) Experimental: (a) ref. 6; (b) ref. 7; (c) this work.

square deviations  $\delta P$ ,  $\delta T$ ,  $\delta x$  and  $\delta y$  between the true value of each experimental variable and the corresponding measured value. Figure 1 compares the calculated results with the experimental data for the three binary systems. The ternary VLE prediction was performed by using the

## TABLE 5

Ternary ca	alculated	results f	or the system	1-butanol (	(1)-acetonitrile	(2)-benzene	(3)	at 60°	°C
						(-)	<u><u> </u></u>		

	Vapor	mole fract	ion ( $\times 10^3$ )	Pressure	
	$\overline{\delta y_1}$	<b>δ</b> y <sub>2</sub>	$\delta y_3$	δP (Torr)	<u>δ</u> <i>P</i> / <i>P</i> (%)
Mean deviation	4.8	3.2	5.0	3.86	1.02
Root-mean-square deviation	5.8	3.9	6.3	5.11	1.36



Fig. 2. Equilibrium tielines.

model having the binary parameters alone and good agreement is observed between the calculated values and the experimental results as indicated in Table 5. Figure 2 shows the tielines connecting the liquid and vapor-phase mole fractions, demonstrating that no ternary azeotrope is present.

### LIST OF SYMBOLS

A, B, C	1-butanol, acetonitrile and benzene
$a_{II}$	binary interaction parameter
$B_{II}$	second virial coefficient
$h_{\Lambda}^{ii}$	enthalpy of hydrogen-bond formation
$h_{AB}, h_{AC}$	enthalpies of formation of chemical complexes A <sub>i</sub> B and A <sub>i</sub> C

K <sub>A</sub>	association constant, $(\Phi_A B / \Phi_A \Phi_A)[i/(i+1)]$
K <sub>AB</sub>	solvation constant between alcohol <i>i</i> -mer and component B to
ΛD	form chemical complex A, B, $(\Phi_{A,P}/\Phi_{A,Q},\Phi_{P})[i/(ir_{A}+r_{P})]$
K	solvation constant between alcohol <i>i</i> -mer and component C to
AC	form chemical complex A C $(\Phi, \alpha/\Phi, \Phi_{\alpha})[i/(ir, +r_{\alpha})]$
Р	total pressure
$P_I^s$	vapor pressure of pure component I
$q_1$	molecular area parameter of pure component I
Ŕ	universal gas constant
$r_{I}$	molecular size parameter of pure component I
T	absolute temperature
V	true molar volume of alcohol mixture
$V^0_{a}$	true molar volume of pure alcohol liquid
$v_L^{L}$	pure-liquid molar volume of component I
$\dot{x_I}$	liquid-phase mole fraction of component I
$\dot{y}_{I}$	vapor-phase mole fraction of component I
Ż	coordination number, equal to 10

## Greek letters

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$\gamma_I$	activity coefficient of component I
$\theta_I$	area fraction of component I
$\sigma_P, \sigma_T$	standard deviations in pressure and temperature
$\sigma_{v}, \sigma_{v}$	standard deviations in liquid- and vapor-phase mole fractions
$ au_{IJ}$	coefficient as defined by $exp(-a_{IJ}/T)$
$\Phi_I$	segment fraction of component I
$\phi_I$	fugacity coefficient of component $I$ at $P$ and $T$
$\phi_I^s$	fugacity coefficient of pure component I at $P_I^s$ and T

## Superscripts

<sup>0</sup> pure-liquid	reference	state
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- liquid L
- saturation s

# **Subscripts**

- 1-butanol, acetonitrile and benzene A, B, C  $A_1, A_1$ monomer and *i*-mer of 1-butanol A, B, A, C complex formation between 1-butanol *i*-mer and component B or С complexes formed by A and B or C AB, AC  $\begin{array}{l} \mathbf{B}_1, \, \mathbf{C}_1 \\ I, \, J, \, K \end{array}$ monomers of components B and C
- components

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