ISOTHERMAL VAPOR-LIQUID EQUILIBRIA FOR BINARY AND TERNARY MIXTURES FORMED BY l-BUTANOL, ACETONITRILE AND BENZENE

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ABSTRACT

Isothermal vapor-liquid equilibrium data are presented for the binary acetonitrile-1-butanol and ternary 1-butanol-acetonitrile-benzene systems at 60" C. The experimental results are well correlated with the UNIQUAC associated-solution model.

INTRODUCTION

Studies on the thermodynamic properties of 1-butanol solutions are currently under way in this laboratory. A literature survey [l-5] showed that isothermal vapor-liquid equilibrium (VLE) data for ternary systems containing 1-butanol are a very few. This work presents isothermal VLE data for the systems acetonitrile-1-butanol and l-butanol-acetonitrile-benzene at 60°C. The VLE data for the two binary systems constituting the ternary system had been measured: acetonitrile-benzene at 45°C [6] and lbutanol-benzene at 45°C [7]. The measured results are well correlated with the UNIQUAC associated-solution model [8].

EXPERIMENTAL

Acetonitrile and l-butanol (Nakarai Pure Chemical Industries Ltd., Analytical reagent grade) were used without further purification. C.P. benzene was subjected to repeated recrystallization. An Anton Paar densimeter (DMA40) was used to measure densities of the compounds. Gas chromatographic analysis did not detect any appreciable impurities in the chemicals. Table 1 shows values of densities and vapor pressures of the compounds, together with literature values [6,9].

An all-glass Boublik vapor-recirculation still [lo] was used to obtain the VLE data. Refractive index measurements were carried out for composition

Compound	Density at 25° C (g cm ⁻³)		Vapor pressure at 60° C (Torr)	
	Obs.	Lit. $[9]$	Obs.	Lit. $[9]$
1-Butanol	0.8059	0.8060	59.1	59.01
Acetonitrile	0.7766	0.7766	368.1	368.00(6)
Benzene	0.8736	0.8737	391.5	391.47

TABLE 1

determination of binary vapor and liquid-phase sample solutions by using a Shimadzu refractometer at 25°C. Ternary sample solutions were analyzed by combining use of a gas chromatograph (Shimadzu GC-8A) and an electronic integrator (Shimadzu Chromatopac E-1A). The experimental errors involved in the measured variables were as follows: 0.16 Torr for pressure; 0.05 K for temperature; 0.002 mole fraction for liquid and vaporphase compositions.

RESULTS AND DISCUSSION

The measured VLE results at 60° C are presented for the binary system acetonitrile-l-butanol in Table 2 and for the ternary system l-butanolacetonitrile-benzene in Table 3.

The experimental data were reduced by use of the relation

$$
P\phi_I y_I = \gamma_I x_I P_I^s \phi_I^s \exp\left[v_I^L (P - P_I^s)/RT\right]
$$
 (1)

where *P* is the total pressure, γ is the activity coefficient, x and y are the liquid- and vapor-phase mole fractions, *Ps* is the pure-component vapor pressure at equilibrium absolute temperature *T* and v^L is the pure-liquid molar volume and was calculated from the modified Rackett equation [ll].

TABLE 2

Vapor-liquid equilibrium data for the system acetonitrile (1) -1-butanol (2) at 60° C

TABLE 3 TABLE 3

Vapor-liquid equilibrium data for the system 1-butanol (1)-acetonitrile (2)-benzene (3) at 60° C Vapor-liquid equilibrium data for the system 1-butanol (1) -acetonitrile (2) -benzene (3) at 60° C

The fugacity coefficients, ϕ_I at *P* and ϕ_I^s at *P_i*, were calculated from the relation

$$
\ln \phi_I = \left(2\sum_J y_J B_{IJ} - \sum_I \sum_J y_I y_J B_{IJ}\right) \frac{P}{RT}
$$
\n(2)

where the second virial coefficient B_{IJ} were estimated from the correlation of Hayden and O'Connell [12].

The UNIQUAC associated-solution model [8] gives the activity coefficients of l-butanol (A), acetonitrile (B) and benzene **(C)** as follows:

$$
\ln \gamma_{A} = \ln \left(\frac{\Phi_{A_{1}}}{\Phi_{A_{1}}^{0} x_{A}} \right) + r_{A} \left(\frac{1}{V_{A}^{0}} - \frac{1}{V} \right) - \left(\frac{Z}{2} \right) q_{A} \left[\ln \left(\frac{\Phi_{A}}{\theta_{A}} \right) + 1 - \frac{\Phi_{A}}{\theta_{A}} \right]
$$

$$
+ q_{A} \left[1 - \ln \left(\sum_{J} \theta_{J} \tau_{JA} \right) - \sum_{J} \frac{\theta_{J} \tau_{A,J}}{\sum_{K} \theta_{K} \tau_{KJ}} \right]
$$
(3)
$$
\ln \gamma_{B} = \ln \left(\frac{\Phi_{B_{1}}}{x_{B}} \right) + 1 - \frac{r_{B}}{V} - \left(\frac{Z}{2} \right) q_{B} \left[\ln \left(\frac{\Phi_{B}}{\theta_{B}} \right) + 1 - \frac{\Phi_{B}}{\theta_{B}} \right]
$$

$$
+ q_{B} \left[1 - \ln \left(\sum_{J} \theta_{J} \tau_{JB} \right) - \sum_{J} \frac{\theta_{J} \tau_{BJ}}{\sum_{K} \theta_{K} \tau_{KJ}} \right]
$$
(4)

and $\ln \gamma_C$ is expressed by changing the suffix B to C in eqn. (4). Z is the coordination number equal to 10. The nominal segment fraction Φ_I , the overall surface fraction θ_I and the adjustable parameter τ_{II} are indicated by

$$
\Phi_I = r_I x_I / \sum_J r_J x_J \tag{5}
$$

$$
\theta_I = q_I x_I / \sum_J q_J x_J \tag{6}
$$

$$
\tau_{JI} = \exp(-a_{JI}/T) \tag{7}
$$

The true molar volume of the ternary mixture is expressed as

$$
\frac{1}{V} = \frac{\Phi_{A_1}}{r_A(1 - K_A \Phi_{A_1})} + \frac{\Phi_{B_1}}{r_B} \left[1 + \frac{K_{AB} r_B \Phi_{A_1}}{(1 - K_A \Phi_{A_1})} \right] + \frac{\Phi_{C_1}}{r_C} \left[1 + \frac{K_{AC} r_C \Phi_{A_1}}{(1 - K_A \Phi_{A_1})} \right]
$$
(8)

The monomeric segment fractions of all the components, Φ_{A_1} , Φ_{B_1} and Φ_{c} , are numerically solved from eqns. (9-11).

$$
\Phi_{A} = \frac{\Phi_{A_1}}{(1 - K_A \Phi_{A_1})^2} \left[1 + r_A (K_{AB} \Phi_{B_1} + K_{AC} \Phi_{C_1}) \right]
$$
(9)

$$
\Phi_{\mathbf{B}} = \Phi_{\mathbf{B}_{\mathbf{I}}} \left[1 + \frac{r_{\mathbf{B}} K_{\mathbf{A}\mathbf{B}} \Phi_{\mathbf{A}_{\mathbf{I}}}}{\left(1 - K_{\mathbf{A}} \Phi_{\mathbf{A}_{\mathbf{I}}}\right)} \right]
$$
(10)

$$
\Phi_{\rm C} = \Phi_{\rm C_1} \left[1 + \frac{r_{\rm C} K_{\rm AC} \Phi_{\rm A_1}}{(1 - K_{\rm A} \Phi_{\rm A_1})} \right]
$$
\n(11)

At pure alcohol state $\Phi_{A_1}^0$ and V_A^0 are derived from eqns. (12) and (13), respectively.

$$
\Phi_{A_1}^0 = \left[2K_A + 1 - (1 + 4K_A)^{1/2}\right] / 2K_A^2
$$
\n
$$
\frac{1}{\sqrt{1 - (1 + K_A)^{1/2}}} = (1 - K_A)^{1/2} \tag{12}
$$

$$
\frac{1}{V_{\rm A}^0} = (1 - K_{\rm A} \Phi_{\rm A_1}^0)/r_{\rm A}
$$
\nThe pure component structured parameters were calculated according to

The pure-component structural parameters were calculated according to the method of Vera et al. [13]: for 1-butanol, $r = 2.77$ and $q = 2.42$; for acetonitrile, $r = 1.50$ and $q = 1.40$; for benzene, $r = 2.56$ and $q = 2.05$. The association constant for 1-butanol K_A is 69.5 at 50°C [14]. The enthalpy of hydrogen-bond formation for the alcohol h_A is -23.2 kJ mol⁻¹ [15]. The values of the solvation constant and the enthalpy of complex formation are $K_{\text{AB}} = 40$ at 50°C and $h_{\text{AB}} = -17$ kJ mol⁻¹ for 1-butanol-acetonitrile and $K_{AC} = 2.5$ at 50°C and $h_{AC} = -8.3$ kJ mol⁻¹ [8]. h_A , h_{AB} and h_{AC} were assumed to be independent of temperature. The temperature dependence of the equilibrium constants were described by the van't Hoff relation.

An optimum set of the parameters for the binary VLE results were obtained by use of a computer program similar to that described by Prausnitz et al. [16]. Standard deviations for the measured variables used in data reduction were $\sigma_p = 1$ Torr for pressure, $\sigma_T = 0.05$ K for temperature, $\sigma_r = 0.001$ for liquid-phase mole fraction and $\sigma_r = 0.003$ for vapor-phase mole fraction. Table 4 shows the results obtained in fitting the UNIQUAC associated-solution model to the binary VLE results and the root-mean-

Binary calculated results of vapor-liquid equilibrium data reduction

Fig. 1. Vapor-liquid equilibria for: (a) acetonitrile (1)-benzene (2) at 45° C; (b) 1-butanol (1)-benzene (2) at 45° C; (c) acetonitrile (1)-benzene (2) at 60° C. (----) Calculated. (.) Experimental: (a) ref. 6; (b) ref. 7; (c) this work.

square deviations δP , δT , δx and δy between the true value of each experimental variable and the corresponding measured value. Figure 1 compares the calculated results with the experimental data for the three binary systems. The ternary VLE prediction was performed by using the

TABLE 5

Fig. 2. Equilibrium tielines.

model having the binary parameters alone and good agreement is observed between the calculated values and the experimental results as indicated in Table 5. Figure 2 shows the tielines connecting the liquid and vapor-phase mole fractions, demonstrating that no ternary azeotrope is present.

LIST OF SYMBOLS

Greek letters

194

Superscripts

- L liquid
- *S* saturation

Subscripts

- A, B, C 1-butanol, acetonitrile and benzene
- A_1 , A_i monomer and *i*-mer of 1-butanol
- A,B, A,C complex formation between 1-butanol i-mer and component B or C
- AB, AC complexes formed by A and B or C
B₁, C₁ monomers of components B and C
I, J, K components
- monomers of components B and C
- components

REFERENCES

- 1 I. Wichterle, J. Linek and E. H&la, Vapor-Liquid Equilibrium Data Bibliography, Elsevier, Amsterdam, 1973.
- 2 I. Wichterle, J. Linek and E. Hala, Vapor-Liquid Equilibrium Data Bibliography, Supplement I, Elsevier, Amsterdam, 1976.
- 3 I. Wichterle, J. Linek and E. Hala, Vapor-Liquid Equilibrium Data Bibliography, Supplement II, Elsevier, Amsterdam, 1979.
- 4 I. Wichterle, J. Linek and E. Hála, Vapor-Liquid Equilibrium Data Bibliography, Supplement III, Elsevier, Amsterdam, 1982.
- 5 I. Wichterle, J. Linek and E. Hgla, Vapor-Liquid Equilibrium Data Bibliography, Supplement IV, Elsevier, Amsterdam, 1985.
- 6 I. Brown and F. Smith, Aust. J. Chem., 8 (1955) 62.
- 7 I. Brown and F. Smith, Aust. J. Chem., 12 (1959) 407.
- 8 I. Nagata, Fluid Phase Equilibria, 19 (1985) 153.
- 9 J.A. Riddick and W.B. Bunger, Organic Solvents, 3rd edn., Wiley-Interscience, New York, 1970, pp. 107, 151, 399.
- 10 I. Nagata, J. Chem. Eng. Data, 30 (1985) 201.
- 11 C.F. Spencer and R.P. Danner, J. Chem. Eng. Data, 17 (1972) 236.
- 12 J.G. Hayden and J.P. O'Connell, Ind. Eng. Chem., Process Des. Dev., 14 (1975) 209.
- 13 J.H. Vera, S.G. Sayegh and G.A. Ratcliff, Fluid Phase Equilibria, 1 (1977) 113.
- 14 V. Brandani, Fluid Phase Equilibria, 12 (1983) 87.
- 15 R.H. Stokes and C. Burfitt, J. Chem. Thermodyn., 5 (1973) 623.
- 16 J.M. Prausnitz, T.F. Anderson, E.A. Grens, C.A. Eckert, R. Hsieh and J.P. O'Connell, Computer Calculations for Multicomponent Vapor-liquid and Liquid-liquid Equilibria, Prentice-Hall, Englewood Cliffs, NJ, 1984, Chaps. 3, 4 and 6 and Appendices C and D.